

オープンCAEシンポジウム2012@岐阜



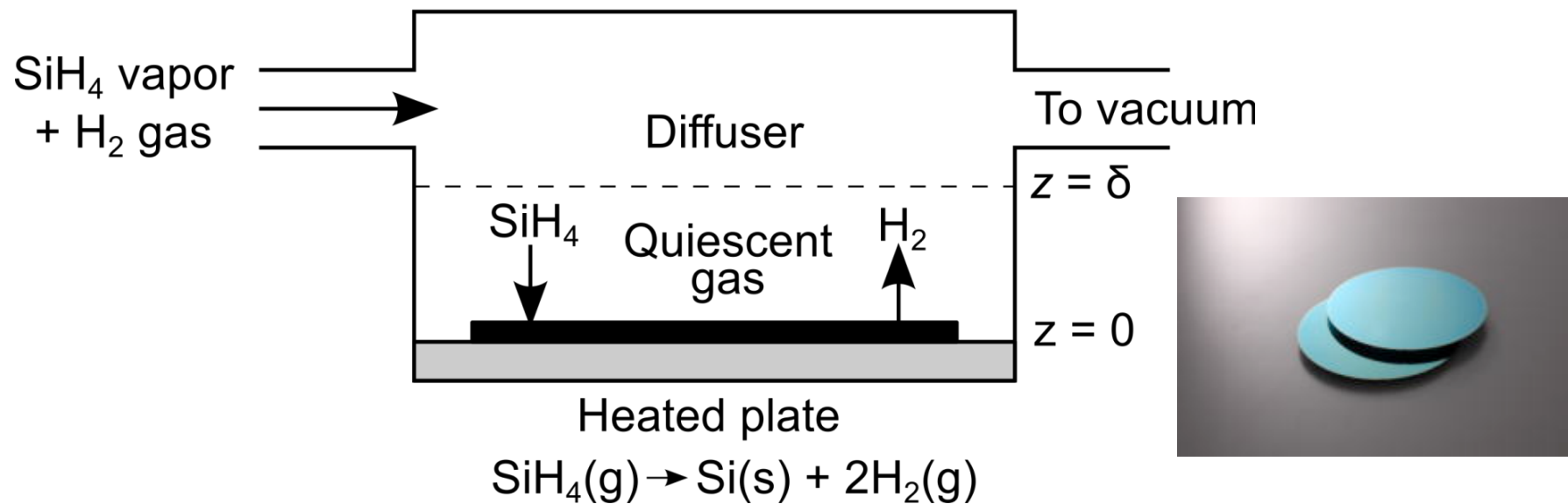
熱物質移動を含むプロセスへの オープンCAEの活用

大阪大学大学院基礎工学研究科

高木 洋平

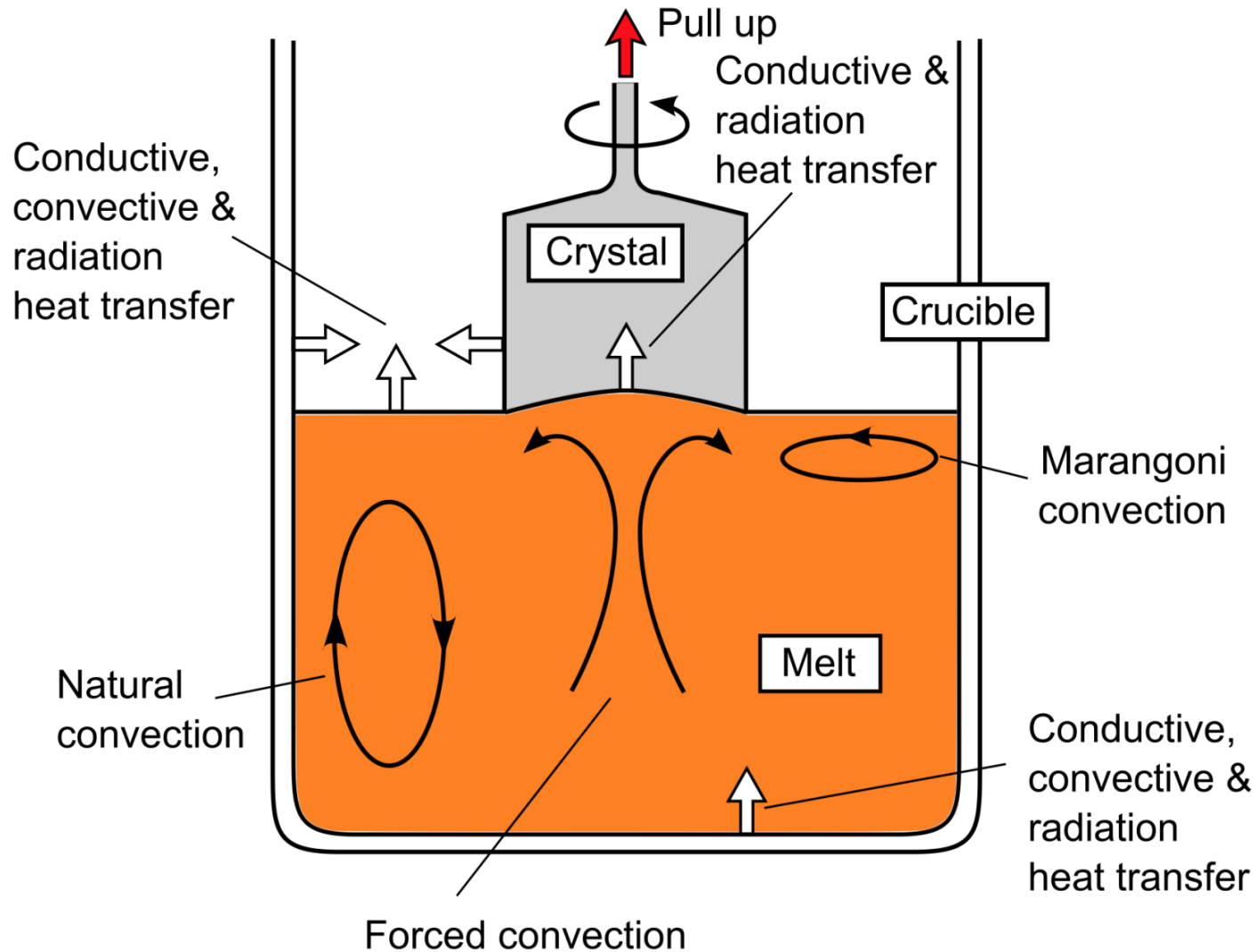
Chemical engineering process

Ex. Chemical Vapor Deposition (CVD)



Heat, Mass and momentum transfer

Transport phenomena in melt





Governing equations in melt

- Navier-Stokes eq.

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\frac{1}{\rho} \nabla P + \nu \nabla^2 \mathbf{u} + \mathbf{F}$$

- Energy eq.

$$\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T = \alpha \nabla^2 T$$

- Diffusion eq.

$$\frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla C = D \nabla^2 C$$

\mathbf{u} : vector
 T : scalar
 C : scalar

Common operator:

Gradient, Divergence, Laplacian, Time Advancement



Advantage of open source

- OpenFOAM
 - Object Oriented Programming

```
grad(T)  
grad(U)
```

Operator overload
Class module



Easy extension

- Fortran code
 - Procedural Programming

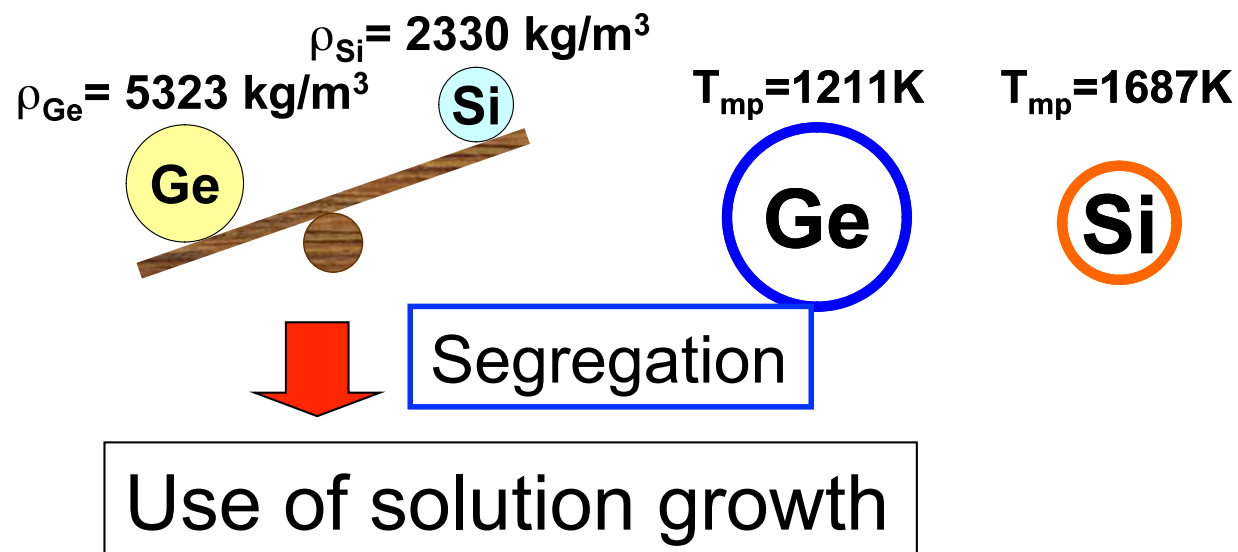
```
call grad(T,dTdx,dTdy,dTdz)  
call grad(u,dudx,dudy,dudz)  
call grad(v,dvdx,dvdy,dvdz)  
call grad(w,dwdx,dwdv,dwdz)
```

Mixture of scalar, vector
and tensor

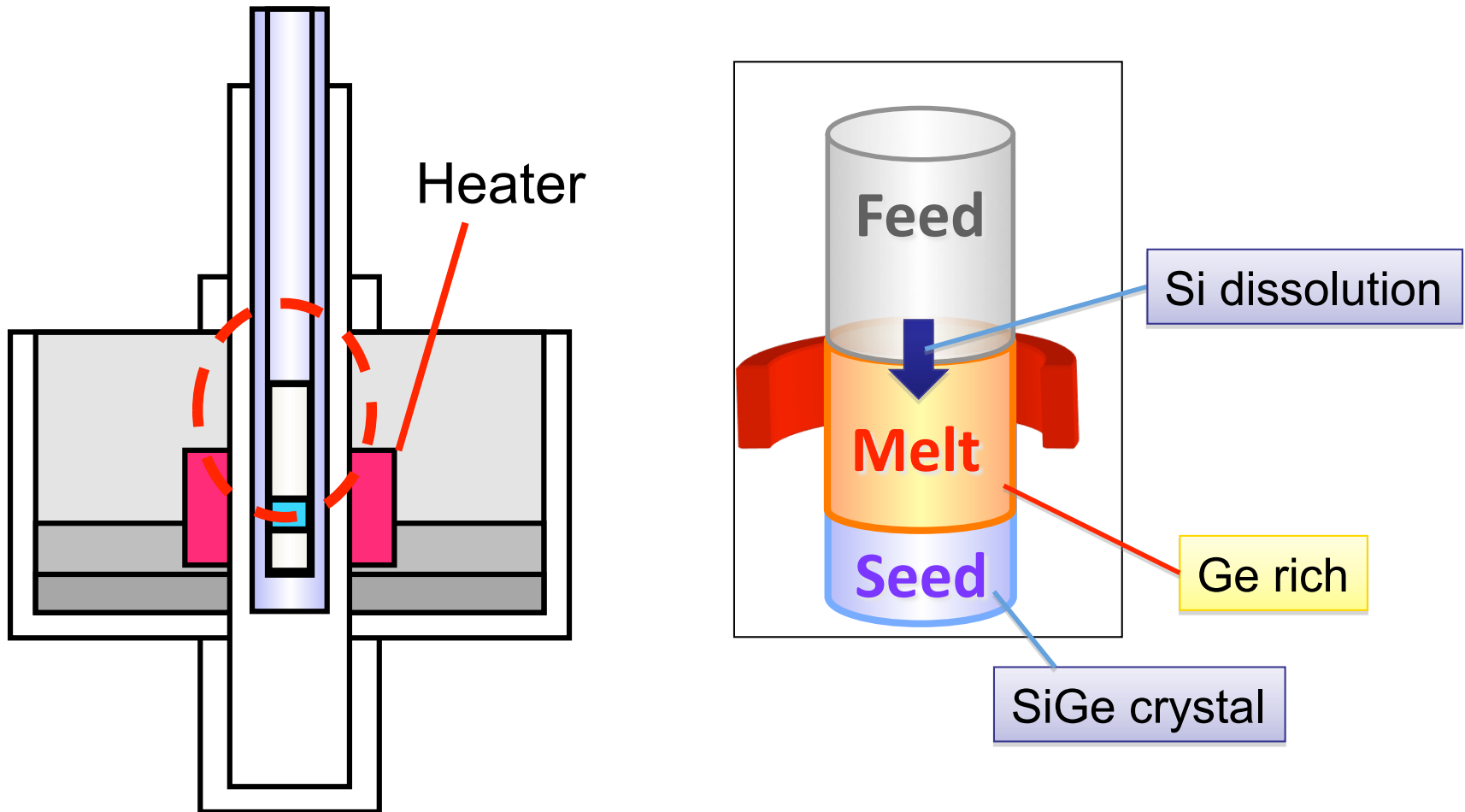


Crystal growth of compound semiconductor

- Silicon germanium (SiGe)
 - $(\text{Si}_x\text{Ge}_{1-x})$
 - High performance, high efficiency
 - Lattice mismatch in Si+SiGe
- Property of SiGe



Traveling Heater Method (THM)

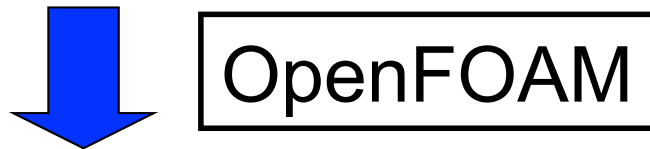


Melt convection with heat and mass transfers

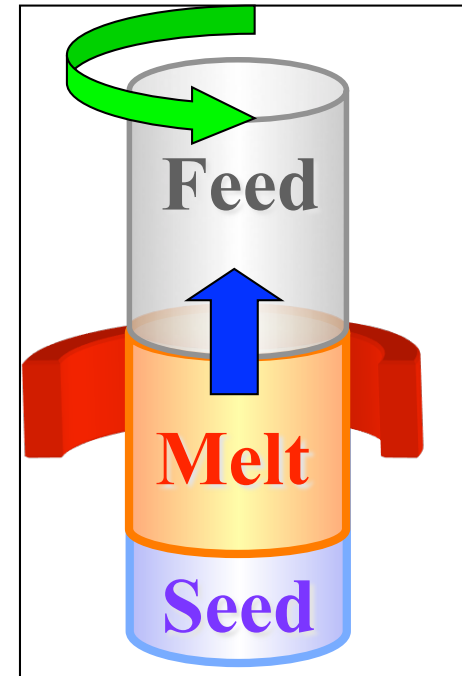


Objective

- Convection control in THM
 - Magnetic field
 - Crucible rotation



- Convection suppression effect with external forces
- Operating condition for high quality crystal
 - Si concentration near growth interface





Governing equations in melt

- Navier-Stokes eq.

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\frac{1}{\rho} \nabla P + \nu \nabla^2 \mathbf{u} + \mathbf{S} + \mathbf{F}$$

$$\mathbf{S} = (\beta_T g(T - T_0) - \beta_C g(C - C_0)) \mathbf{e}_Z \quad \mathbf{F} = \mathbf{J} \times \mathbf{B}$$

- Induction eq. of magnetic field

$$\frac{\partial \mathbf{B}}{\partial t} + \nabla \cdot (\mathbf{u} \times \mathbf{B} - \mathbf{B} \times \mathbf{u}) - \nabla \cdot \frac{1}{\sigma \mu} \nabla \mathbf{B} = 0$$

- Energy eq.

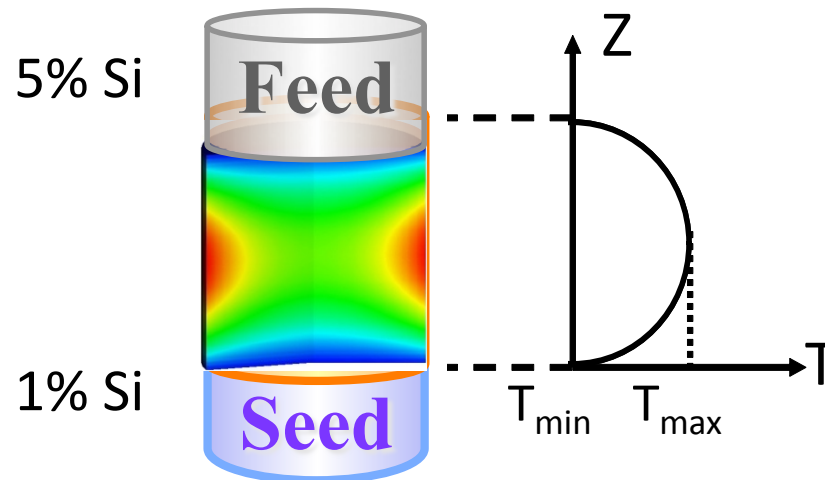
$$\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T = \alpha \nabla^2 T$$

- Diffusion eq.

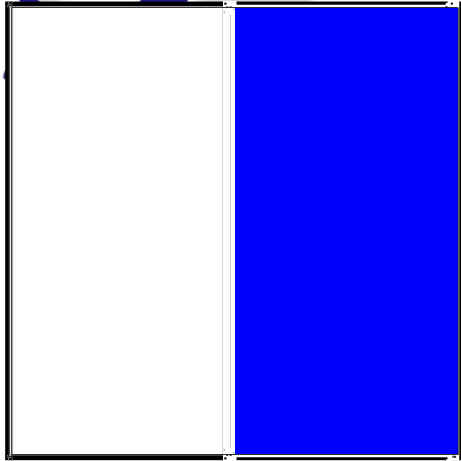
$$\frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla C = D \nabla^2 C$$

Boundary condition

- Velocity: no-slip condition, rotating wall velocity
- Magnetic field : static vertical
- Temperature and concentration:



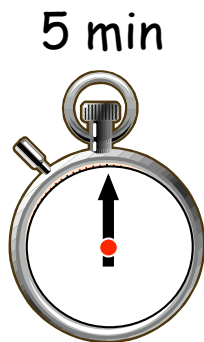
- Not considered: moving boundary of crystal-melt surface, heater movement



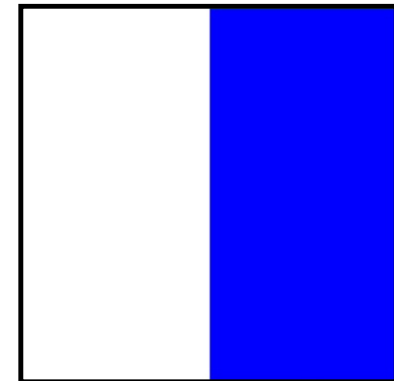
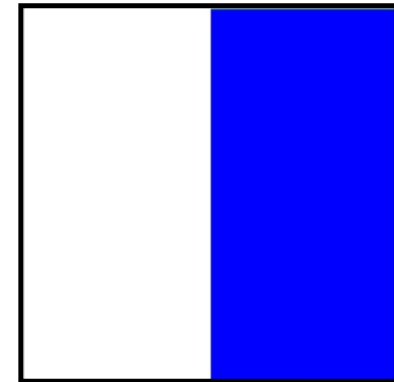
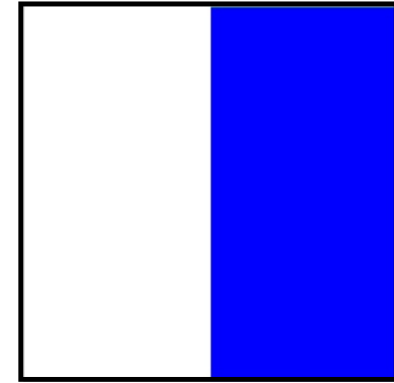
Si concentration [%]
1.0 5.0

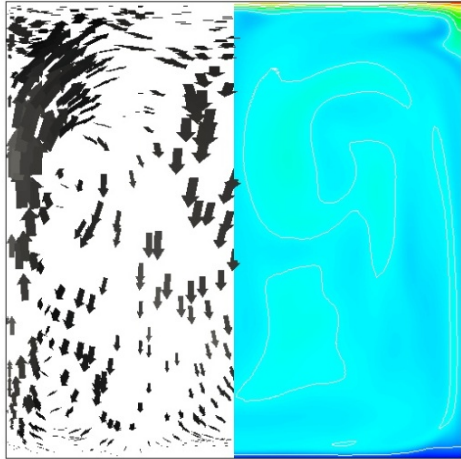
No control

	M.F.	Rot.
Case1	×	×
Case2	○	×
Case3	×	○
Case4	○	○



With Magnetic field

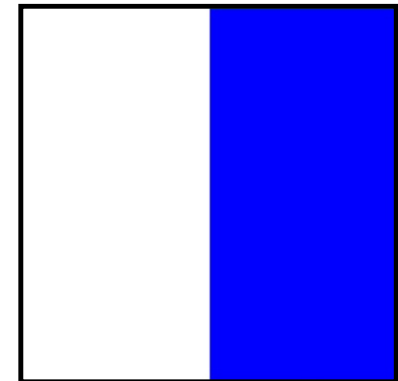
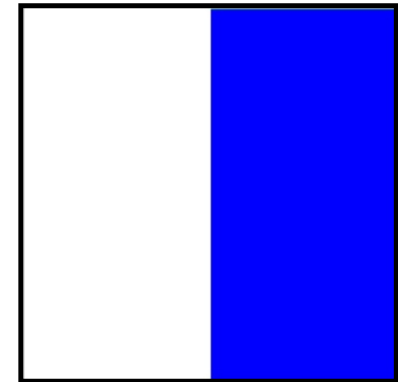
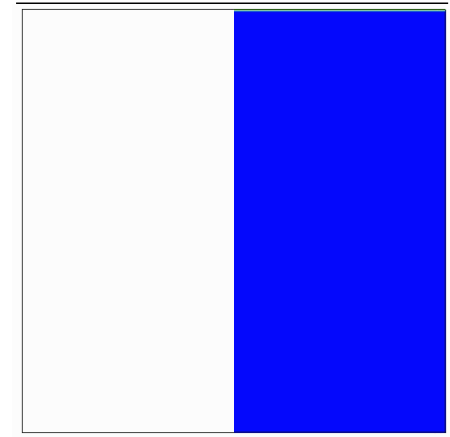
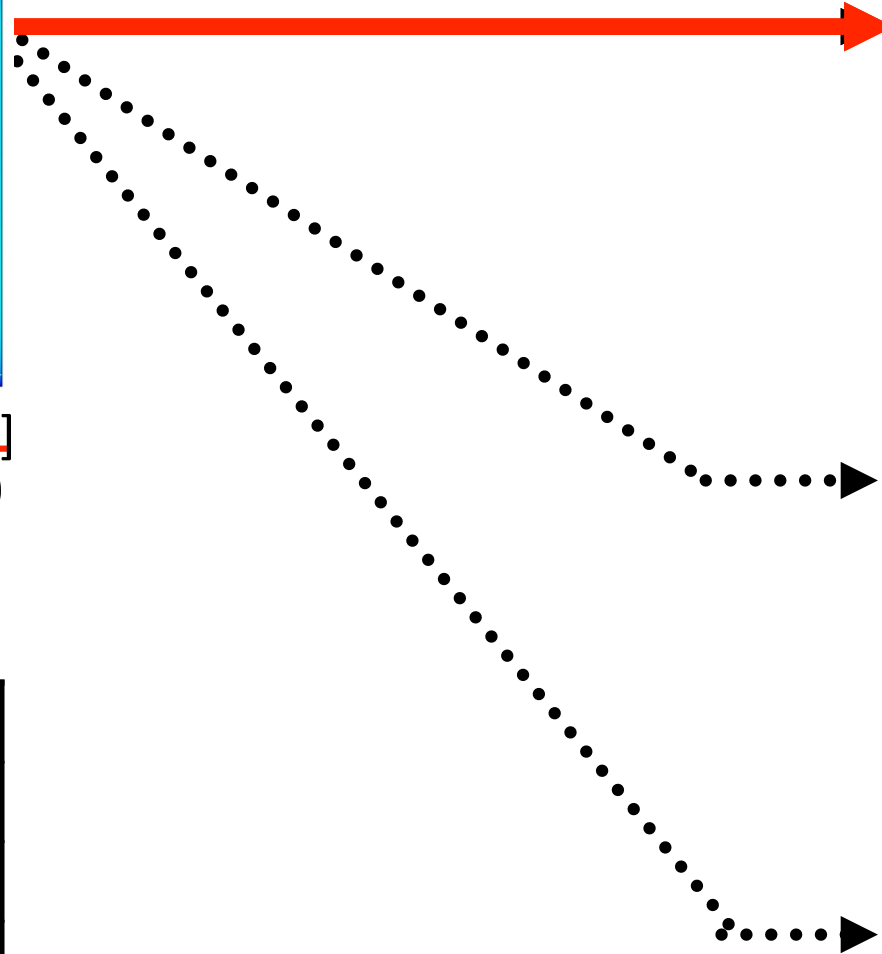




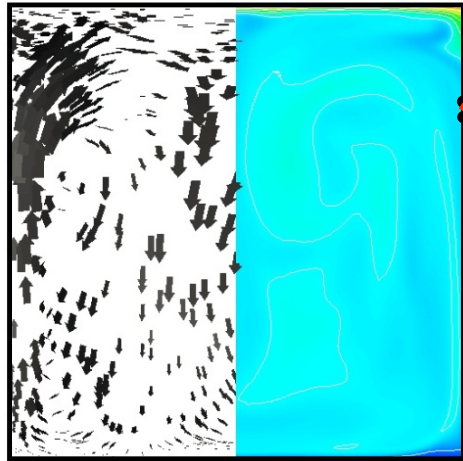
Si concentration [%]
 1.0 5.0

No control

With Magnetic field



	M.F.	Rot.
Case1	×	×
Case2	○	×
Case3	×	○
Case4	○	○

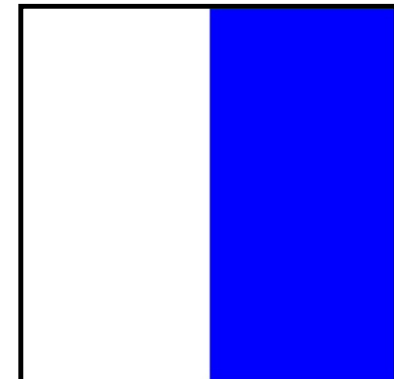
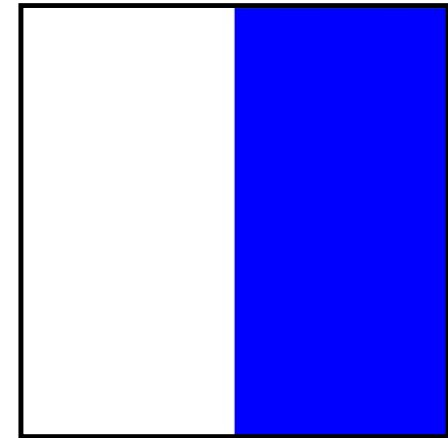
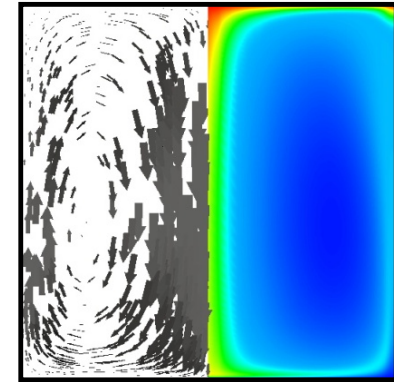


Si concentration [%]
 1.0 5.0

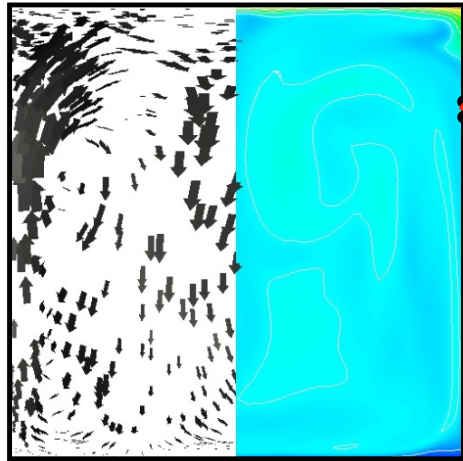
With Magnetic field

$V_{max}=1.04$ m/s
 $V_z_{max}=0.07$ m/s

With rotation



	M.F.	Rot.
Case1	×	×
Case2	○	×
Case3	×	○
Case4	○	○



Si concentration [%]

1.0 5.0



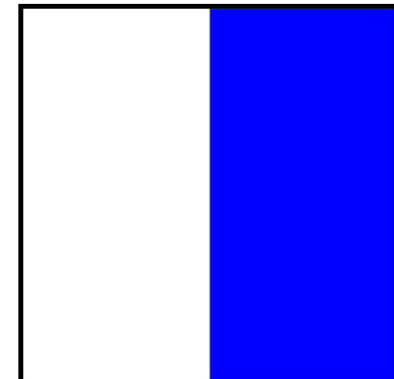
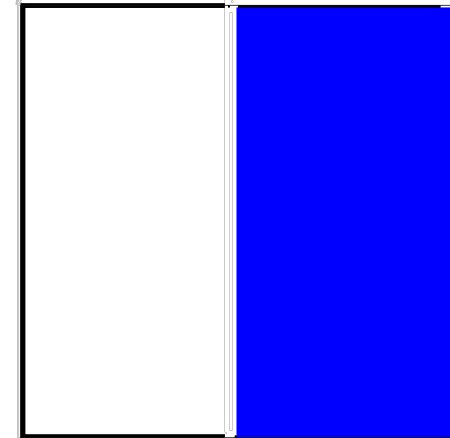
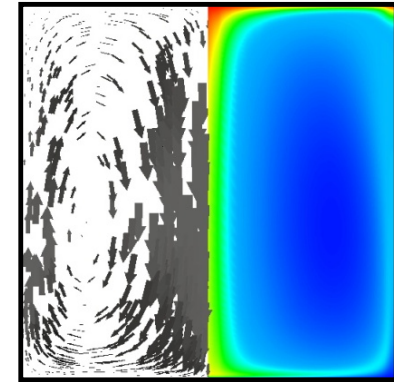
$V_z = 6.4 \times 10^{-3}$ m/s

With Magnetic field

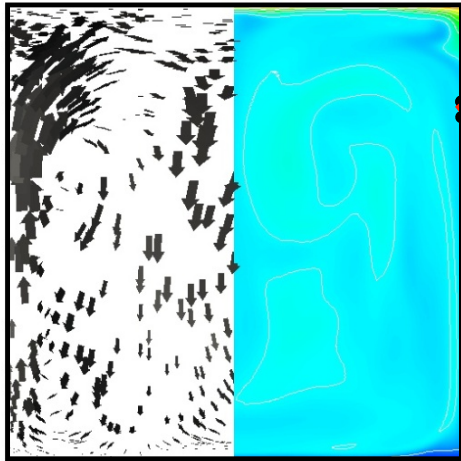
$V_{max} = 1.04$ m/s

$V_{z,max} = 0.07$ m/s

With rotation



	M.F.	Rot.
Case1	×	×
Case2	○	×
Case3	×	○
Case4	○	○

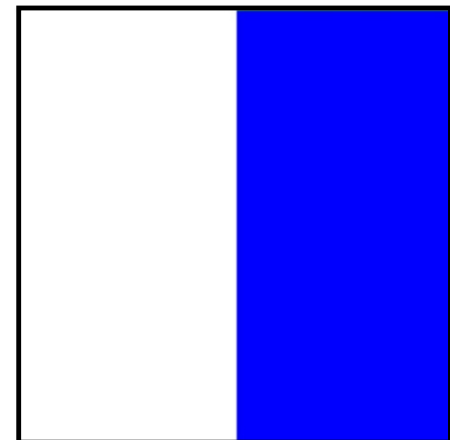
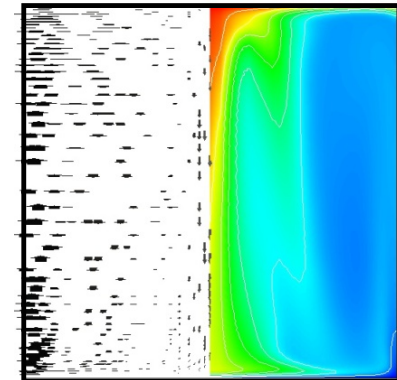
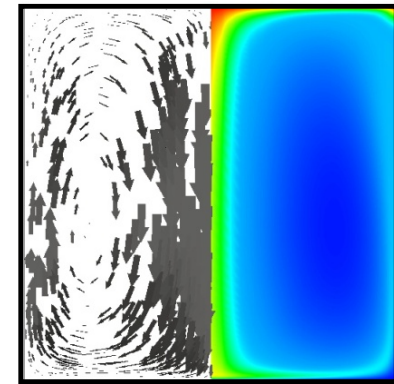


Si concentration [%]
1.0 5.0

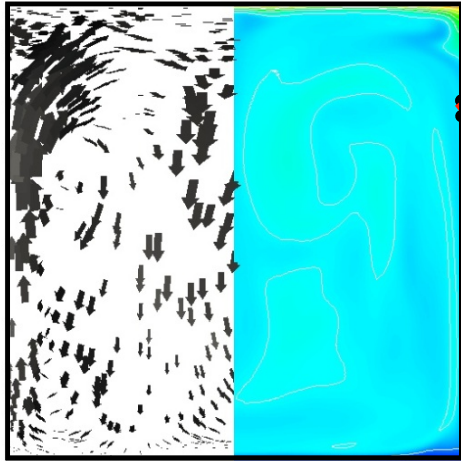
With Magnetic field

With rotation

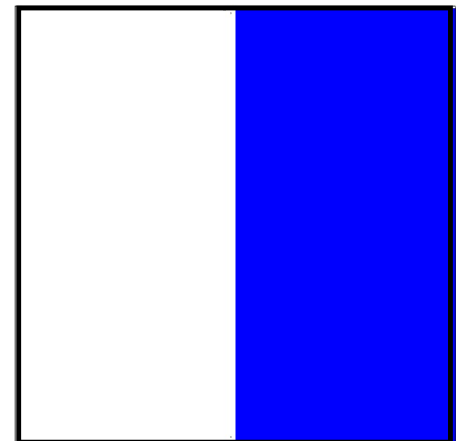
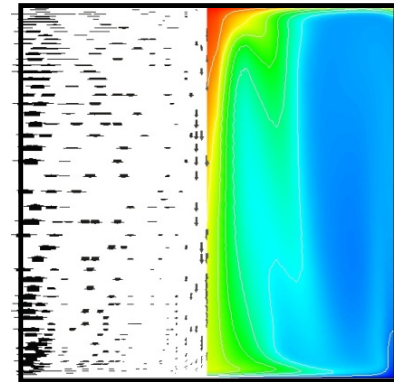
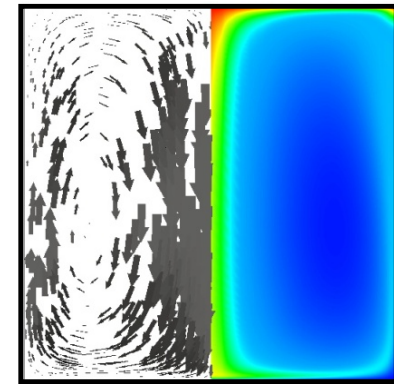
With rotation
& Magnetic field



	M.F.	Rot.
Case1	×	×
Case2	○	×
Case3	×	○
Case4	○	○

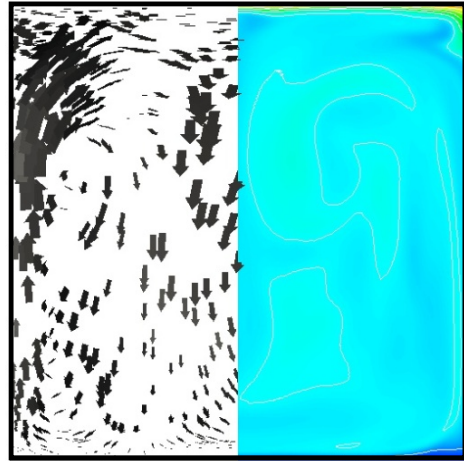


Si concentration [%]
1.0 5.0

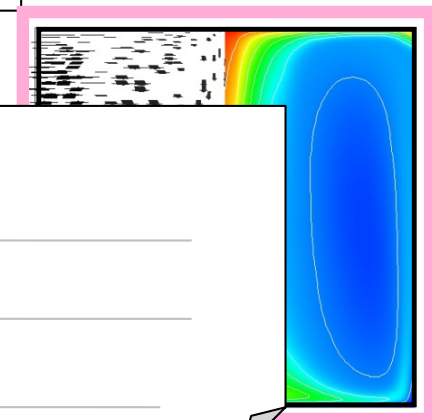
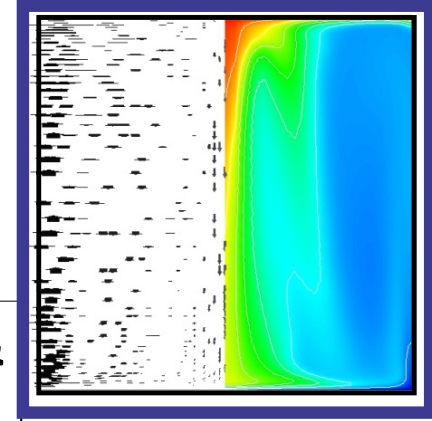
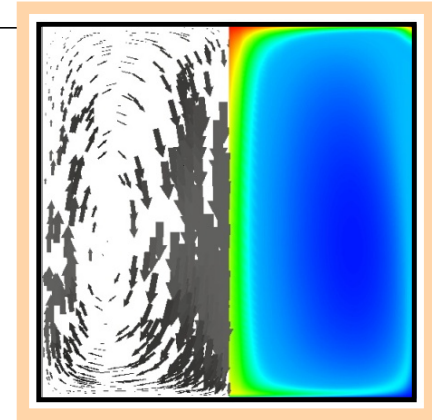
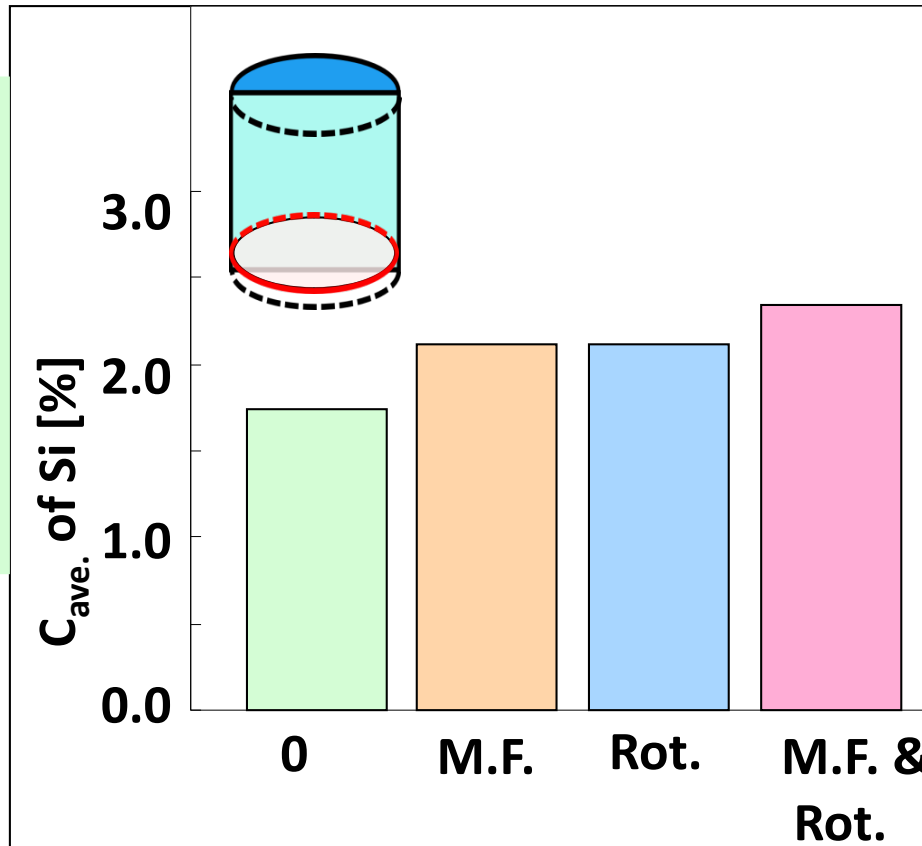


	M.F.	Rot.
Case1	×	×
Case2	○	×
Case3	×	○
Case4	○	○

**With rotation
& Magnetic field**



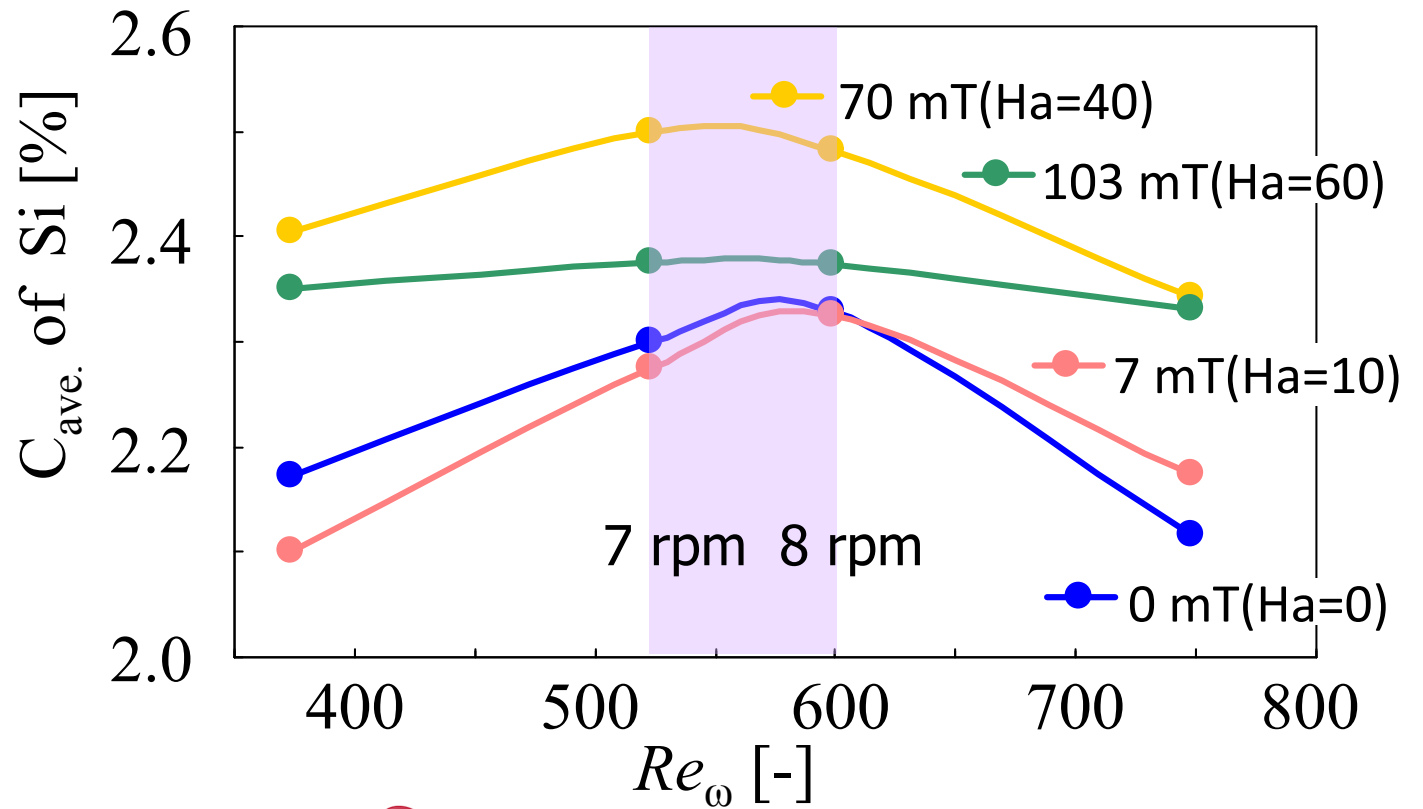
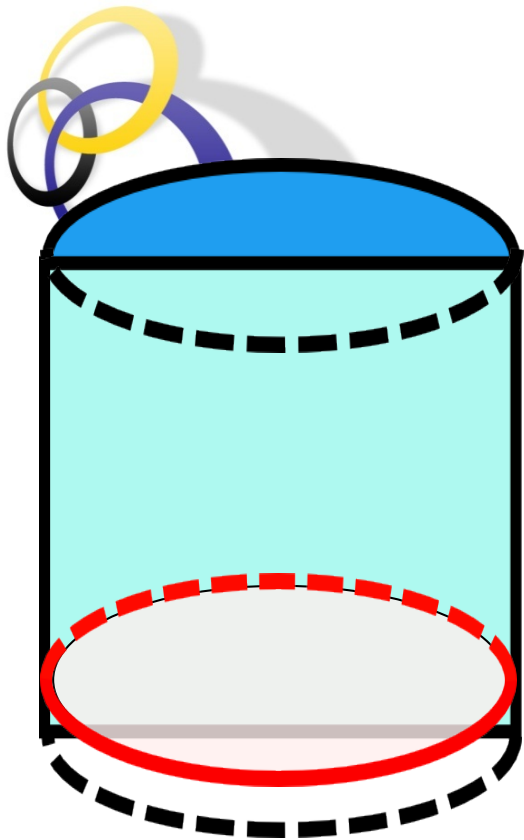
Si concentration [%]
1.0 5.0



	M.F.	Rot.
Case		
Case		
Case		
Case		

★ *Combination of M.F. and rotation*

↻ *Rich Si near growth interface*

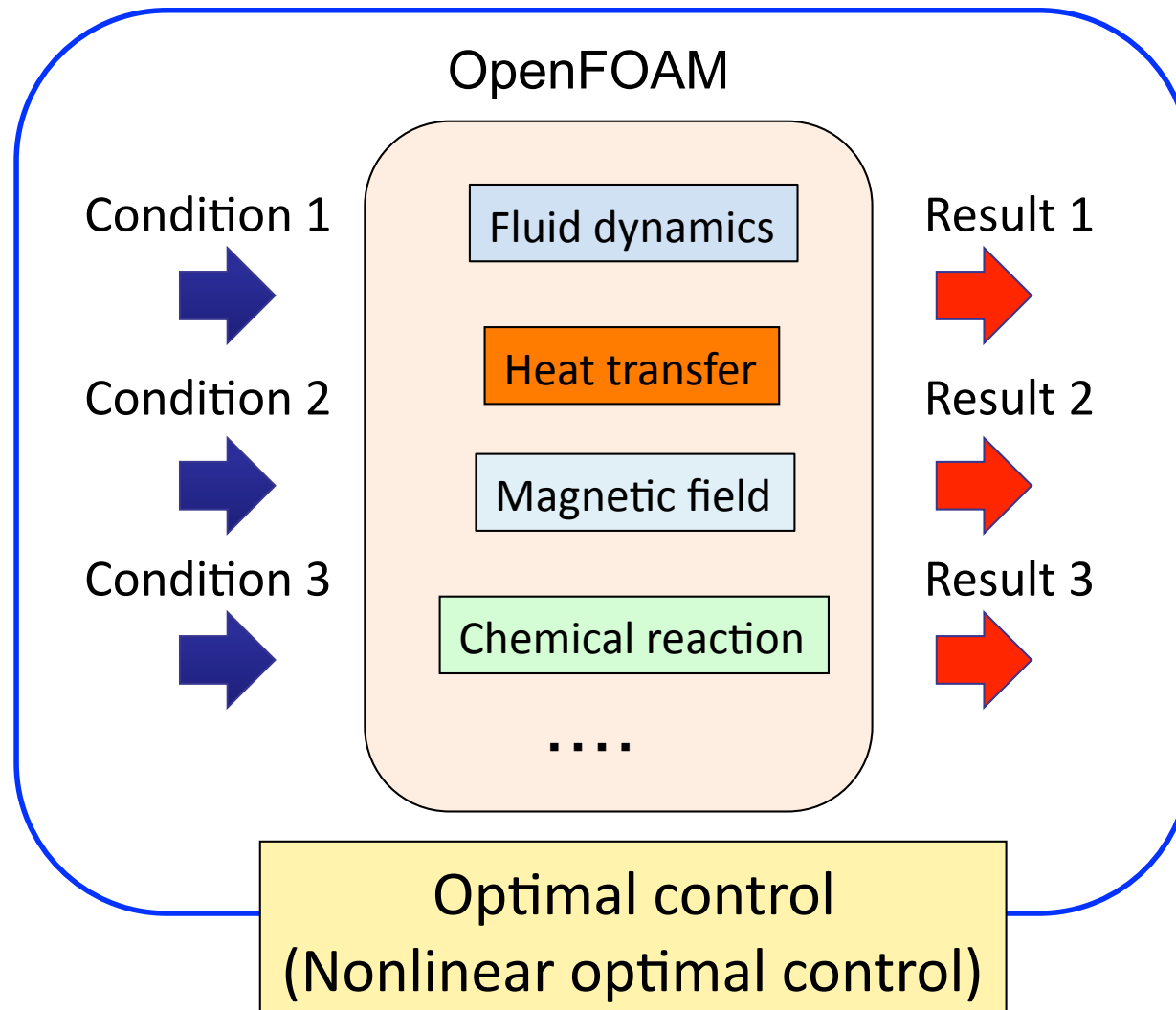


★ *Combination of M.F. and rotation*
7-8 rpm & around 70mT(Ha=40)

↻ *Rich Si near growth interface*

Best

Toward smart control





First step for smart control: Adjoint method

Adjoint method formulation for ducted flow

- Adjoint N-S equations:

$$-2D(\mathbf{u})\mathbf{v} = -\nabla q + \nabla \cdot (2\nu D(\mathbf{u})) - \alpha \mathbf{u}$$

$$\nabla \cdot \mathbf{u} = 0$$

- Adjoint BCs for the wall and inlet:

$$\mathbf{u}_t = 0, \quad u_n = -\frac{\partial J_\Gamma}{\partial p}$$

$$\mathbf{n} \cdot \nabla q = 0$$

- Adjoint BCs for the outlet:

$$q = \mathbf{u} \cdot \mathbf{v} + u_n v_n + \nu (\mathbf{n} \cdot \nabla) u_n + \frac{\partial J_\Gamma}{\partial v_n}$$

$$0 = v_n \mathbf{u}_t + \nu (\mathbf{n} \cdot \nabla) \mathbf{u}_t + \frac{\partial J_\Gamma}{\partial \mathbf{v}_t}$$



Ex. 1: Dissipated power

Cost function:

$$J := - \int_{\Gamma} d\Gamma \left(p + \frac{1}{2} v^2 \right) \mathbf{v} \cdot \mathbf{n}$$

$$J_{\Omega} = 0, \quad J_{\Gamma} = - \left(p + \frac{1}{2} v^2 \right) \mathbf{v} \cdot \mathbf{n}$$

Derivatives for BCs:

$$\frac{\partial J_{\Gamma}}{\partial p} = - \mathbf{v} \cdot \mathbf{n},$$

$$\frac{\partial J_{\Gamma}}{\partial \mathbf{v}} = - \left(p + \frac{1}{2} v^2 \right) \mathbf{n} - (\mathbf{v} \cdot \mathbf{n}) \mathbf{v}$$

Adjoint BCs for the wall and inlet:

$$\mathbf{u}_t = 0 \quad \text{at wall}$$

$$u_n = \begin{cases} 0 \\ v_n \end{cases} \quad \text{at inlet}$$

Adjoint BCs for the outlet:

$$q = \mathbf{u} \cdot \mathbf{v} + u_n v_n + \nu (\mathbf{n} \cdot \nabla) u_n - \frac{1}{2} v^2 - v_n^2$$

$$0 = v_n (\mathbf{u}_t - \mathbf{v}_t) + \nu (\mathbf{n} \cdot \nabla) \mathbf{u}_t$$



OSAKA UNIVERSITY

adjointShapeOptimization.C

```
// Adjoint Pressure-velocity SIMPLE corrector
```

```
{
```

```
    // Adjoint Momentum predictor
```

```
    volVectorField adjointTransposeConvection((fvc::grad(Ua) & U));
```

```
    zeroCells(adjointTransposeConvection, inletCells);
```

```
    tmp<fvVectorMatrix> UaEqn
```

```
    (
```

```
        fvm::div(-phi, Ua)
```

$\nabla \cdot (-\phi \mathbf{u})$

```
    - adjointTransposeConvection
```

$-\nabla \mathbf{u} \cdot \mathbf{v}$

```
    + turbulence->divDevReff(Ua)
```

$-\nabla \cdot (2\nu D(\mathbf{u}))$

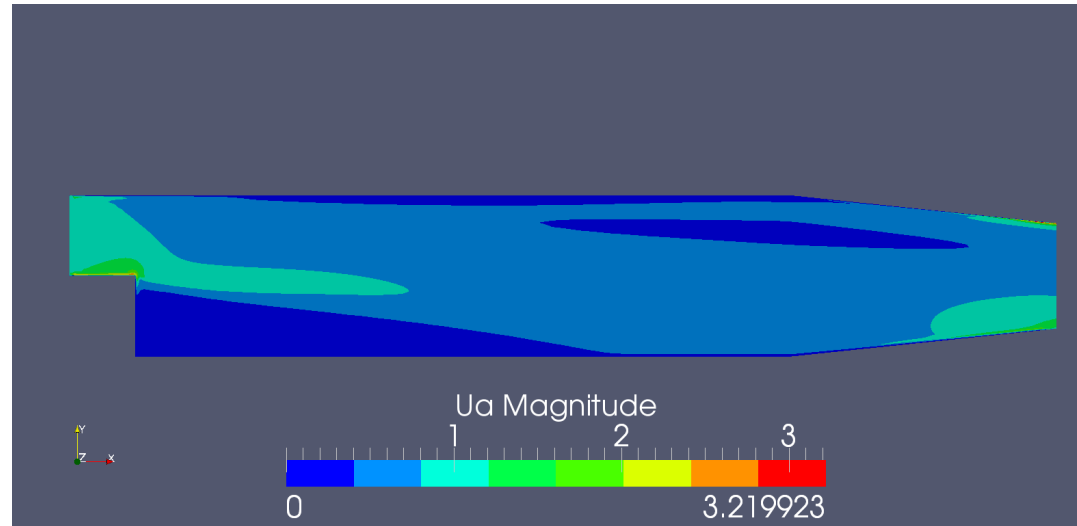
```
    + fvm::Sp(alpha, Ua)
```

$+\alpha \mathbf{u}$

```
);
```



Result: adjoint velocity





Summary

- The simulation including heat, mass and momentum transfers is carried out by using OpenFOAM.
- OpenFOAM is suitable for multi-physics problem.
- Simulation code for optimization is now developed.